Material Property Testing of Polymethyl-Methacrylate (PMMA)

John Oertel, Frank Lopez and Philip Rae, Andrew Hime

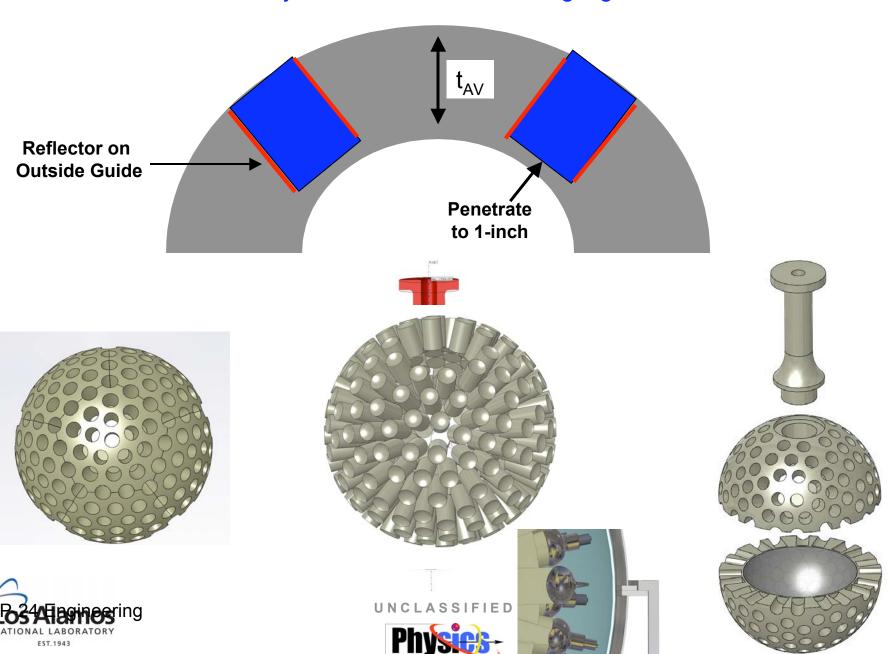
January 22, 2008



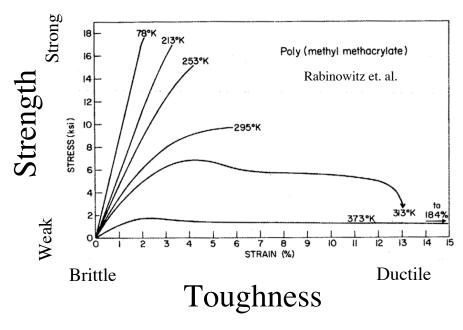




Thick Acrylic Vessel with Penetrating Light Guides



PMMA behaves very differently depending on the operating temperature



PMMA can show all the features of a glassy, brittle solid or an elastic rubber or a viscous liquid depending on the temperature. At low temperature PMMA may be glass like with a high Young's modulus and will break or flow with strains greater that 5%. At high temperatures the same PMMA may be rubber like with a lower modulus without permanent deformation. At higher temperatures still, permanent deformation occurs under load and the material behaves like a highly viscous liquid.



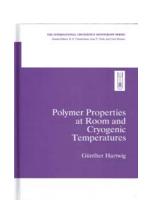


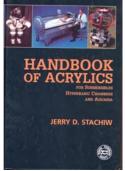
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Mechanical properties of interest as a function of temperature

Young's Modulus - E Shear Modulus - G Poisson's ratio - υ Coefficient of thermal expansion - α Thermal conductivity - k Yield strength - σ Molecular weight - M_n





⁶ P.I. Vincent, Polymer, 1, P.425 (1960)







^{1.} Low Temperature Elastic Moduli and Internal Dilational and Shear Friction of Polymethyl Methacrylate, Mikio Fukuhara and Asao Sampei, J of Polymer Sci B, 33, 1847-1850 (1995)

² G. Hartwig, Polymer Properties at Room and Cryogenic Temperatures, Plenum Press, NY, p.266 (1994)

^{3.} Craze formation and fracture in glassy polymers, S. Rabinowitz et.al., Crit Rev Macromol Sci, 1, P.1 (1972)

^{4.} Jerry Stachiw, Handbook of Acrylics, Best Publishing, Flagstaff, AZ (2003)

⁵ J.E. Graebner et. al., Phys. Rev. B Vol. 34, 8, P. 5696 (1986)

Young's Modulus also called modulus of elasticity or tensile modulus (GPa)

Young's modulus describes the material's response to linear strain (like pulling on the ends of a wire). As the temperature drops, PMMA has a Young's modulus that changes from 7.2 to 8.2 GPa (300 to 2.4 K).^{1,2}

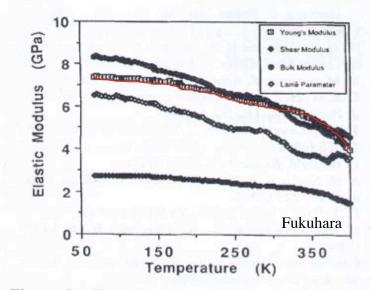


Figure 2. Young's, shear, and bulk moduli and Lamè parameter of polymethyl methacrylate as a function of temperature.

$$E = \frac{\sigma}{\varepsilon} = \frac{F/A_0}{\Delta L/L_0} = \frac{FL_0}{A_0 \Delta L}$$

PMMA 7.2 - 8.2 Gpa_(G.H.) SS 304 195 Gpa Aluminum 60 GPa







Shear Modulus also called modulus of rigidity (GPa)

The shear modulus describes the material's response to shearing strains. the Shear modulus increases from 1.7 to 2.9 GPa from temperatures 300 K to 2.4 K.

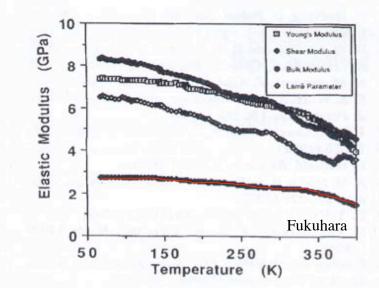


Figure 2. Young's, shear, and bulk moduli and Lamè parameter of polymethyl methacrylate as a function of temperature.

$$G = \frac{E}{2(1+\nu)}$$

PMMA 1.7 - 2.9 Gpa SS 304 73 Gpa Aluminum 27 GPa







Poisson's ratio tends to increase as temperature drops from 0.33 - 0.35 over temperatures 300 to 50 K.

The ratio of transverse (lateral) strain to the corresponding longitudinal (axial) strain.

PROPERTIES OF POLYMETHYL METHACRYLATE

1849

$$\upsilon = rac{arepsilon_{lat}}{arepsilon_{long}}$$

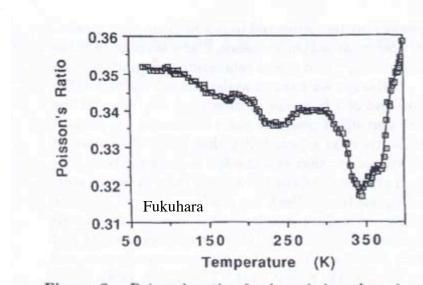


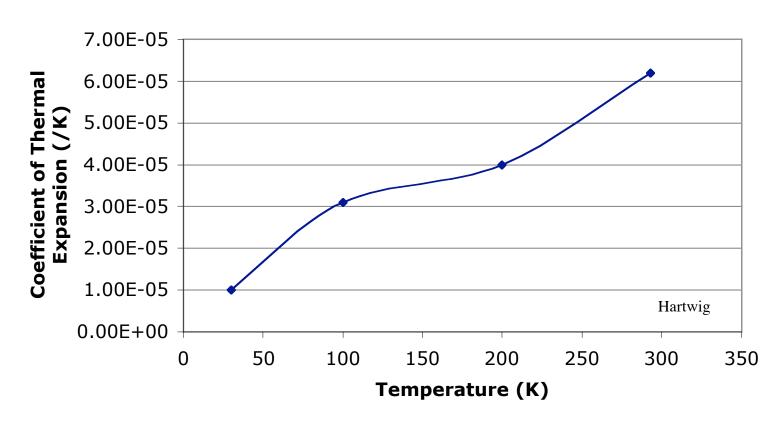
Figure 3. Poisson's ratio of polymethyl methacrylate as a function of temperature.







Coefficient of thermal expansion for PMMA is significant







PMMA =
$$60 \times 10^{-6}$$

SS = 17.3×10^{-6} @23 C
A1 = 23×10^{-6}

Thermal conductivity decreases as temperature decreases

Defined as the quantity of heat, Q, transmitted in time T through a thickness L, in a direction normal to a surface of area A, due to a temperature difference ΔT , under steady state conditions and when the heat transfer is dependent only on the temperature gradient.

Thermal conductivity of the material drops as the temperature is reduced with values ranging from 0.2 to 0.02 W/m-K over 300 K to 1 K.

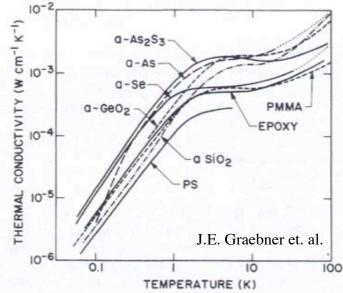


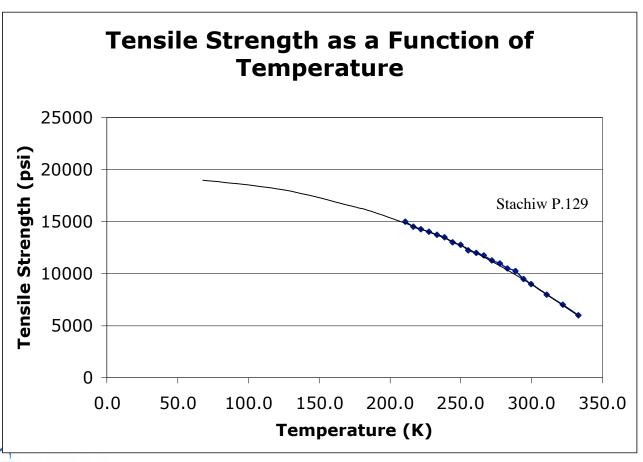
FIG. 1. Thermal conductivity of a-SiO₂ (Ref. 8), a-GeO₂ (Ref. 36), a-As₂S₃ (Refs. 7 and 23), a-As (Ref. 4), a-Se (Ref. 8), epikote epoxy (Ref. 24, sample N), and polymethylmethacrylate (PMMA) and polystyrene (PS) (Ref. 37).





Tensile or yield strength (psi)

What is the value as a function of temperature?



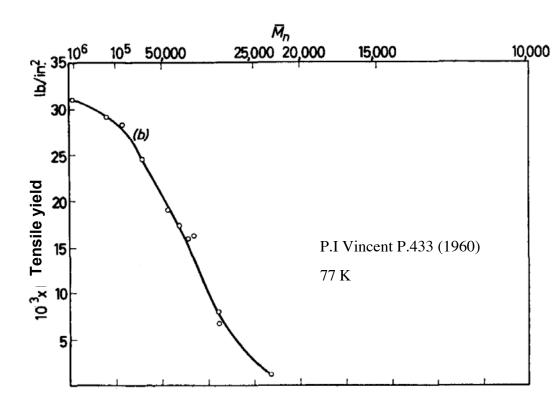
PMMA 10,000 psi SS 304 124,767 psi Aluminum 64,560 psi







The Strength of the material Increases as Molecular Weight Increases



RPT acrylic has an average molecular weight greater than 10⁶, but they also add a cross polymer at a few percent that makes a M_n measurement difficult.



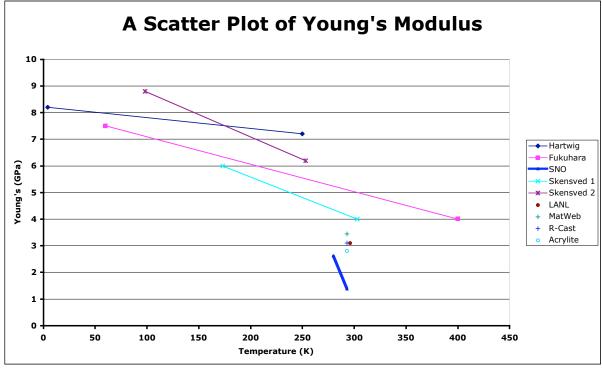




Bottom line...

We will have to measure the mechanical properties of the same PMMA we intend to use.

| Thermal expansion | Temp Range | Reference |
|-----------------------|-------------|--|
| 10 - 62 x10-6/K | 30 - 293K | Gunter Hartwig |
| 6 x 10-5 /C | 296 K | SNO Design Report for AV |
| Thermal Conductivit | Temp Range | Reference |
| 0.02 - 0.2 x10-2 W/m- | -1 - 300 K | Gunter Hartwig |
| 0.005 - 0.2 W/m-K | 0.1 - 100K | Stephens |
| Young's Modulus | Temp Range | Reference |
| 8.2 - 7.2 GPa | 4.2 - 250 K | Gunter Hartwig |
| 7.5 - 4 GPa | 60 - 400 K | Fukuhara |
| 2.62 - 1.38 GPa | 280 - 293 K | SNO Design Report for AV |
| 6 -4 GPa | 173 - 303 K | DMA tests, RPT Acrlylic 4-24-07 Peter Skensved |
| 8.8 - 6.2 GPa | 98 - 253 K | 2nd round of DMA tests 4/07, Peter Skensved |
| 3.1 GPa | 296 K | LANL MST-8 Philip Rae, RPT Acrylic |
| Shear Modulus | Temp Range | Reference |
| 2.9 - 1.7 GPa | 4.2 - 290k | Gunter Hartwig |
| 2.9 - 1.5 GPa | 50 - 400 K | Fukuhara |
| Poisson's Ratio | Temp Range | Reference |
| 0.35 - 0.32 | 60 - 300 K | Fukuhara |
| 0.35 | 296 K | SNO Design Report for AV |
| Tensiile Strength | Temp Range | Reference |
| 9000 psi | 296 K | SNO Design Report for AV |
| 15,000 - 6,000 psi | 211 - 333 K | Stachiw |







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Material Testing is a Core Capability at LANL



MTS880 Material Test System

- •100KN Hydraulic capacity
- •250KN Frame capacity



Specimen in holding fixture



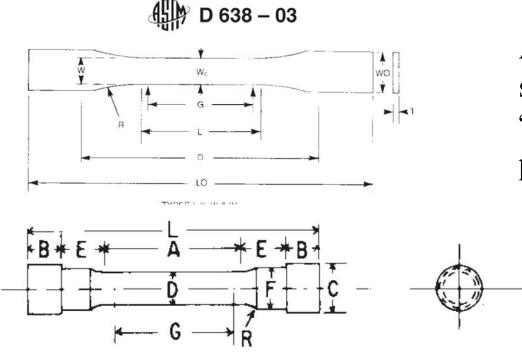
Extensometer in place







Industry has standard test coupons used to benchmark material properties



ASTM D 638-03 is the standard test coupon or "dogbone" used by the plastics industry

ASTM E 8-04 is the standard test coupon or "dumbell" used by the metals industry

The flat dog bone was incompatible with our experimental setup using a cryostat assisted material test system

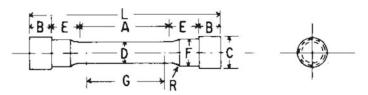




The ASTM E8-04 Failed Outside the Gauge Area











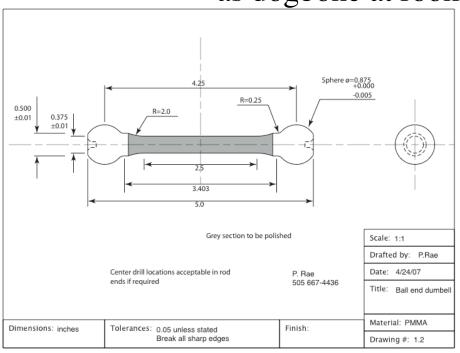


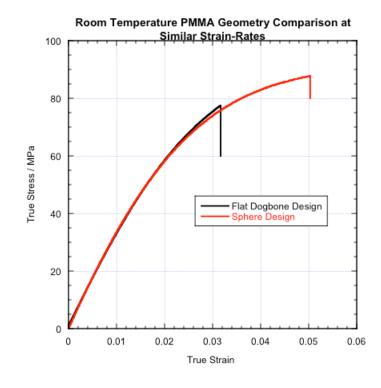




We constructed a "Ball Dumbell" based on the other standards and verified the design with an FEA

Ball dumbell showed same properties as dogbone at room temperature











Ball Dumbell failed where we expected it to!











Testing of RPT PMMA August 6, 2007

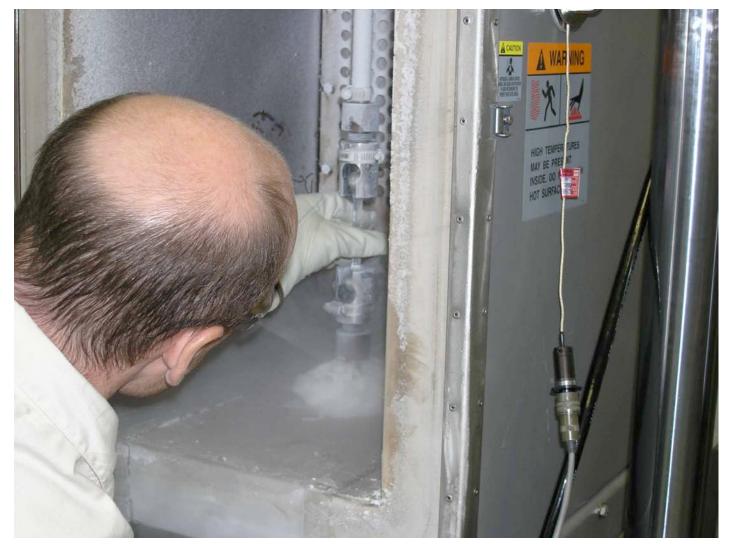
Measurement of tensile strength and Young's modulus Five different temperatures Two different strain rates Comparison between bonded and un-bonded material Five samples for each test = 100 samples Ball ended dumbells

| Bond | Bond | Bond | Bond | Bond |
|----------------------|----------------------|----------------------|----------------------|----------------------|
| Strain rate 10-3/sec |
| 20C | -40C | -100C | -150C | -196C |
| | | | | |
| Bond | Bond | Bond | Bond | Bond |
| Strain rate 10-1/sec |
| 20C | -40C | -100C | -150C | -196C |
| | | | | |
| No Bond |
| Strain rate 10-3/sec |
| 20C | -40C | -100C | -150C | -196C |
| | | | | |
| No Bond |
| Strain rate 10-1/sec |
| 20C | -40C | -100C | -150C | -196C |









MTS Systems Inc. Model 880 with environmental chamber

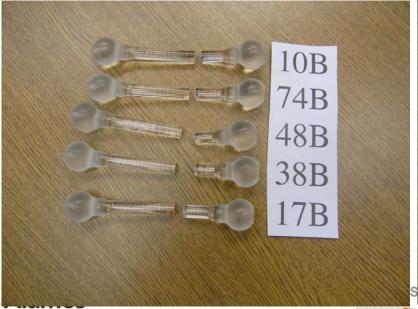




Dumbbells from room temperature tests.









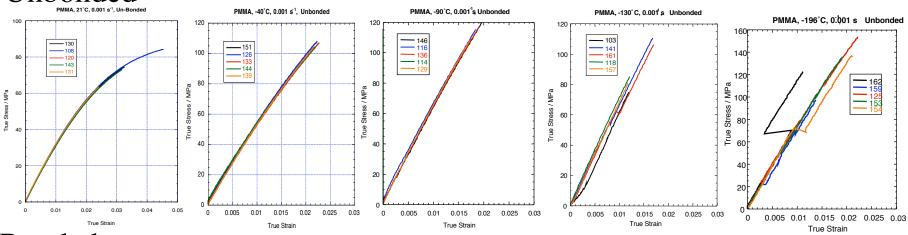




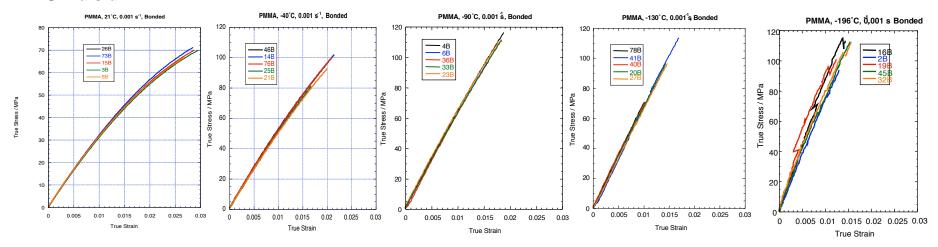


Stress vs. strain graphs, 22, -40, -90, -130, -196 C

Unbonded



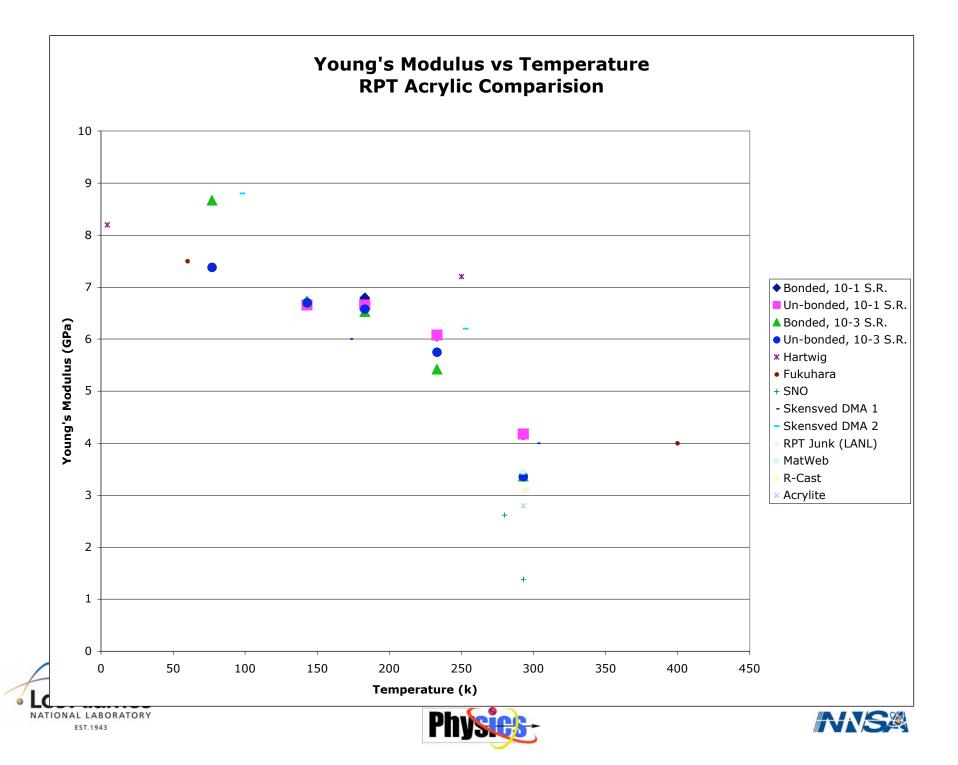
Bonded

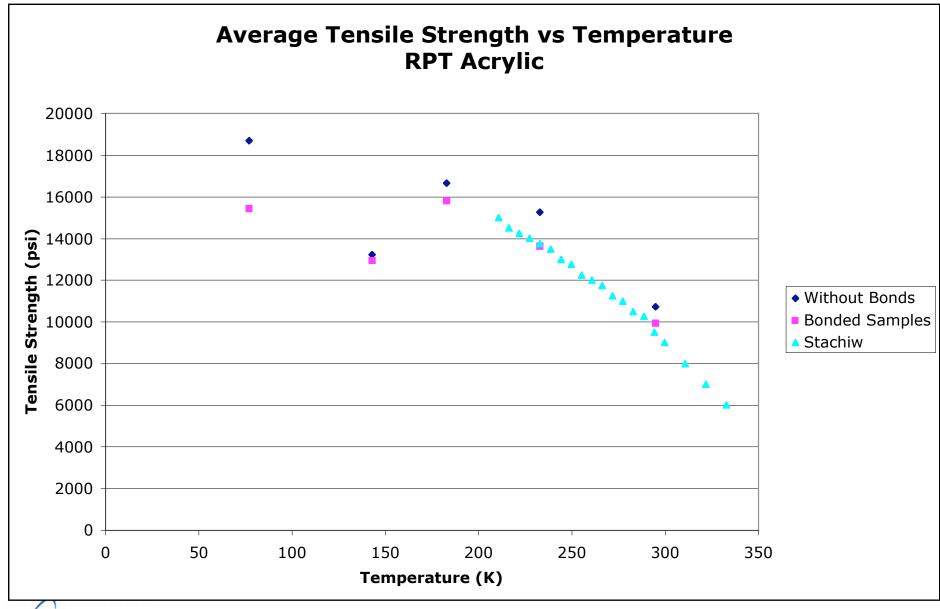


















Factor of Safety (FoS)

Used to provide a design margin over theoretical design capacity to allow for uncertainty in the design process

- Measure of reliability
- •Knowledge of material properties
- •Knowledge of environment
- Accuracy of real loads and wear estimates
- •Consequences of failure
- •Costs
- Safety







| item | Factor of Safety | Application |
|------|------------------|--|
| 1 | 1 25 1 5 | Material properties known in detail. Operating conditions known in detail Loads and resultant stresses and strains known with with high degree of certainty. Material test certificates, proof loading, regular inspection and maintenance. Low weight is important to design. |
| 2 | 1.5 - 2 | Known materials with certification under reasonably constant environmental conditions, subjected to loads and stresses that can be determined using qualified design procedures. Proof tests, regular inspection and maintenance required |
| 3 | 2 - 2.5 | Materials obtained for reputable suppliers to relevant standards operated in normal environments and subjected to loads and stresses that can be determined using checked calculations. |
| 4 | 115-3 | For less tried materials or for brittle materials under average conditions of environment, load and stress. |
| 5 | 3 - 4 | For untried materials used under average conditions of environment, load and stress. |
| 6 | 3 - 4 | Should also be used with better-known materials that are to be used in uncertain environments or subject to uncertain stresses. |

Repeated Cyclic loads:

The factors established above must be based on the endurance limit (fatigue strength) rather than to the yield strength of the material. The strength calculations should also include for stress concentration factors.

Impact Shock forces:

The factors given in items 3 to 6 are acceptable, but an impact factor (the above dynamic magnification factor) should be included.

Brittle materials:

The ultimate strength is used as the theoretical maximum, the factors presented in items 1 to 6 should be approximately doubled. (6-8)







Conclusions

- •Although RPT does a good job bonding acrylic, the bonds are always weaker than the parent material. At -196, bonds are 20% weaker on average.
- •Acrylic does get stronger at low temp, but it's more brittle and dominated by fracture toughness. (Flaws and imperfections will be nucleation points for failure)
- •Construct acrylic vessel in a monolithic pour if possible
- •Keep all acrylic at the same temperature to reduce thermal stress
- •Use most conservative mechanical properties in FEA
- Cool down slowly
- •Use a high FOS
- Test concepts to failure if possible







Raw Data Tables







Tests of RPT PMMA

September-07

Comparison between bonded and non-bonded PMMA dumbbells

21 - 22 C

22 C, 10-1/s

Dumbbell Gauge dimensions

| Experimental Run | Sample # | Dumbbell # | Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Average Young's modulus | Force req. to break (kN) | Top (mm) | Middle (mm) | Bottom (mm) | Average (mm) | min (mm) | max(mm) | Delta (mm) | Comments | Comments |
|------------------|----------|------------|-----------------------|------------------------|------------------------|-------------------------------|--------------------------------|----------|-------------|-------------|--------------|----------|---------|------------|--|---|
| С | 11 | 10B | 10 ⁻¹ /sec | 82.3 | 11936.6274 | | 5.7 | 9.483 | 9.53 | 9.498 | 9.504 | 9.483 | 9.530 | 0.047 | failed at the bond | Sample loaded w/ bond up, Bond stayed in long end |
| | 12 | 74B | 10 ⁻¹ /sec | 83.3 | 12081.6654 | | 5.76 | 9.46 | 9.482 | 9.477 | 9.473 | 9.460 | 9.482 | 0.022 | failed at the bond | Sample loaded w/ bond up, Bond stayed in short end |
| | 13 | 48B | 10 ⁻¹ /sec | 77.7 | 11269.4526 | | 5.27 | 9.329 | 9.409 | 9.343 | 9.360 | 9.329 | 9.409 | 0.080 | failed at the bond | Sample loaded w/ bond up, Bond stayed in long end |
| | 14 | 38B | 10 ⁻¹ /sec | 85.5 | 12400.749 | | 5.91 | 9.52 | 9.561 | 9.537 | 9.539 | 9.520 | 9.561 | 0.041 | failed at the bond | Sample loaded w/ bond up, Bond stayed in long end |
| | 15 | 17B | 10 ⁻¹ /sec | 82.2 | 11922.1236 | | 5.7 | 9.498 | 9.473 | 9.448 | 9.473 | 9.448 | 9.498 | 0.050 | failed at the bond | Sample loaded w/ bond up, Bond stayed in short end |
| | | | ave | 82.2 | 11922.12 | 4.16 | 5.668 | | | | | | | | | |
| D | 16 | 127 | 10 ⁻¹ /sec | 85 | 12328.23 | | 5.9 | 9.514 | 9.641 | 9.533 | 9.563 | 9.514 | 9.641 | 0.127 | failed at the center of gauge | Though the largest diameter sample, it wasn't the highest yield |
| | 17 | 160 | 10 ⁻¹ /sec | 95.5 | 13851.129 | | 6.6 | 9.493 | 9.527 | 9.555 | 9.525 | 9.493 | 9.555 | 0.062 | failed at the root of the gauge | |
| | 18 | 113 | 10 ⁻¹ /sec | 95.1 | 13793.1138 | | 6.54 | 9.538 | 9.547 | 9.514 | 9.533 | 9.514 | 9.547 | 0.033 | failed at the root of the gauge | |
| | 19 | 148 | 10 ⁻¹ /sec | 99.2 | 14387.7696 | | 6.82 | 9.575 | 9.541 | 9.506 | 9.541 | 9.506 | 9.575 | 0.069 | failed at the root of the gauge | |
| | 20 | 111 | 10 ⁻¹ /sec | 83 | 12038.154 | | 5.74 | 9.537 | 9.535 | 9.52 | 9.531 | 9.520 | 9.537 | 0.017 | failed at the tension gauge knife edge | |
| | | | ave | 91.56 | 13279 68 | 4.18 | 6.32 | | | | | | | | | |

-40 C, 10-1/sec

Dumbbell Gauge dimensions

| Experimental Run | Sample # | Dumbbell # | Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Young's modulus (Gpa) | Force req. to break (kN) | Top (mm) | Middle (mm) | Bottom (mm) | Average (mm) | min (mm) | max(mm) | Delta (mm) | Comments | Comments |
|------------------|----------|------------|-----------------------|------------------------|------------------------|-----------------------------|--------------------------------|----------|-------------|-------------|--------------|----------|---------|------------|---|--|
| A | 1 | 1B | 10 ⁻¹ /sec | 107 | 15519.066 | | 7.4 | 9.543 | 9.554 | 9.545 | 9.547 | 9.543 | 9.554 | 0.011 | break at the bond, seperate bond cookie | broke into 3 pieces |
| | 2 | 13B | 10 ⁻¹ /sec | 99.5 | 14431.281 | | 6.9 | 9.466 | 9.48 | 9.514 | 9.487 | 9.466 | 9.514 | 0.048 | break at the bond, seperate bond cookie | broke into 3 pieces |
| | 3 | 5B | 10 ⁻¹ /sec | 106.5 | 15446.547 | | 7.4 | 9.449 | 9.468 | 9.47 | 9.462 | 9.449 | 9.470 | 0.021 | break at bond and into little bits | broke into 5 pieces |
| | 4 | 35B | 10 ⁻¹ /sec | 106.6 | 15461.0508 | | 7.4 | 9.524 | 9.506 | 9.475 | 9.502 | 9.475 | 9.524 | 0.049 | break at bond and into little bits | broke into 8 pieces |
| | 5 | 39B | 10 ⁻¹ /sec | 99.3 | 14402.2734 | | 7 | 9.486 | 9.481 | 9.502 | 9.490 | 9.481 | 9.502 | 0.021 | Bond is intact. Failed at root and in gauge | broke into 3 pieces, forgot to pull pin on strain gauge here |
| | | | ave | 103.78 | 15052.04 | 6.06 | 7.22 | | | | 9.498 | | | | | |
| В | 6 | 119 | 10 ⁻¹ /sec | 112.2 | 16273.2636 | | 7.8 | 9.535 | 9.535 | 9.475 | 9.515 | 9.475 | 9.535 | 0.060 | Broke at root both ends | broke into 4 pieces |
| | 7 | 112 | 10 ⁻¹ /sec | 107.4 | 15577.0812 | | 7.5 | 9.525 | 9.539 | 9.529 | 9.531 | 9.525 | 9.539 | 0.014 | Failed at root of one end | broke into 3 pieces |
| | 8 | 121 | 10 ⁻¹ /sec | 110.5 | 16026.699 | | 7.7 | 9.502 | 9.527 | 9.521 | 9.517 | 9.502 | 9.527 | 0.025 | Broke at root both ends | broke into 3 pieces |
| | 9 | 106 | 10 ⁻¹ /sec | 112.8 | 16360.2864 | | 7.8 | 9.513 | 9.532 | 9.503 | 9.516 | 9.503 | 9.532 | 0.029 | Broke at root both ends | broke into 4 pieces |
| | 10 | 140 | 10 ⁻¹ /sec | 104.8 | 15199.9824 | | 7.3 | 9.528 | 9.544 | 9.529 | 9.534 | 9.528 | 9.544 | 0.016 | Broke at root both ends | broke into 4 pieces |
| | | | ave | 109.54 | 15887.46 | 6.08 | 7.62 | | | | 9,522 | | | | | |

-90C, 10-1/sec

Dumbbell Gauge dimensions

| | | | | Tensile | Tensile | Average Young's | Force req. to break | | | | | | | | | |
|------------------|----------|------------|-----------------------|-------------|-------------|--------------------|------------------------|----------|-------------|-------------|--------------|----------|---------|------------|--|--|
| Experimental Run | Sample # | Dumbbell # | Strain Rate | Yield (Mpa) | Yield (PSI) | modulus | (kN) | Top (mm) | Middle (mm) | Bottom (mm) | Average (mm) | min (mm) | max(mm) | Delta (mm) | Comments | Comments |
| С | 11 | 42B | 10 ⁻¹ /sec | 116.3 | 16867.9194 | | 8.1 | 9.51 | 9.404 | 9.364 | 9.426 | 9.364 | 9.510 | 0.146 | Bond is intact. Failed at both roots | broke into 4 pieces |
| | 12 | 80B | 10 ⁻¹ /sec | 110.7 | 16055.7066 | | 7.7 | 9.553 | 9.558 | 9.555 | 9.555 | 9.553 | 9.558 | 0.005 | break at bond and bond stayed with broken long end | broke into 4 pieces |
| | 13 | 34B | 10 ⁻¹ /sec | 93.2 | 13517.5416 | | 6.5 | 9.498 | 9.496 | 9.464 | 9.486 | 9.464 | 9.498 | 0.034 | break at bond and bond stayed with long end | broke into 2 pieces |
| | 14 | 44B | 10 ⁻¹ /sec | 121.9 | 17680.1322 | | 8.5 | 9.514 | 9.52 | 9.536 | 9.523 | 9.514 | 9.536 | 0.022 | Bond is intact. Failed at both roots | broke into 5 pieces |
| | 15 | 30B | 10 ⁻¹ /sec | 103.5 | 15011.433 | | 7.2 | 9.509 | 9.527 | 9.526 | 9.521 | 9.509 | 9.527 | 0.018 | Bond is intact. Failed at gauge two places | broke into 3 pieces |
| | | | ave | 109.12 | 15826.55 | 6.79 | 7.6 | | | | 9.502 | | | | | |
| D | 16 | 117 | 10 ⁻¹ /sec | 110.1 | 15968.6838 | | 7.1 | 9.553 | 9.562 | 9.551 | 9.555 | 9.551 | 9.562 | 0.011 | Broke in gauge both ends | broke into 3 pieces |
| | 17 | 152 | 10 ⁻¹ /sec | 76.9 | 11153.4222 | | 5.4 | 9.538 | 9.534 | 9.511 | 9.528 | 9.511 | 9.538 | 0.027 | Broke in gauge one end | broke into 3 pieces |
| | 18 | 158 | 10 ⁻¹ /sec | 88.6 | 12850.3668 | | 6.2 | 9.512 | 9.512 | 9.518 | 9.514 | 9.512 | 9.518 | 0.006 | Broke in root and gauge | broke into 5 pieces |
| | 19 | 110 | 10 ⁻¹ /sec | 86.8 | 12589.2984 | | 6.1 | 9.547 | 9.539 | 9.518 | 9.535 | 9.518 | 9.547 | 0.029 | Broke in gauge one end | broke into 2 pieces |
| | 20 | 101 | 10 ⁻¹ /sec | 114.6 | 16621.3548 | | 8 | 9.517 | 9.548 | 9.536 | 9.534 | 9.517 | 9.548 | 0.031 | Broke in root and gauge | broke into 3 pieces, forgot to pull pin on strain gauge here |
| | | | ave | 95.4 | 13836.63 | 6.66 | 6.56 | | | | 9.533 | | | | | |

-130C, 10-1/sec

Dumbbell Gauge dimensions
Average Force reg

| Experimental Run | Sample # | Dumbbell # | Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Young's modulus | to break (kN) | Top (mm) | Middle (mm) | Bottom (mm) | Average (mm) | min (mm) | max(mm) | Delta (mm) | Comments | Comments |
|------------------|----------|------------|-----------------------|------------------------|------------------------|--------------------|------------------|----------|-------------|-------------|--------------|----------|---------|------------|--|---------------------|
| E | 11 | 22B | 10 ⁻¹ /sec | 98.9 | 14344.2582 | | 6.9 | 9.501 | 9.482 | 9.494 | 9.492 | 9.482 | 9.501 | 0.019 | break at bond and bond stayed with short end | broke into 2 pieces |
| | 12 | 7B | 10 ⁻¹ /sec | 98 | 14213.724 | | 6.8 | 9.442 | 9.475 | 9.358 | 9.425 | 9.358 | 9.475 | 0.117 | Bond is intact. Failed at gauge two places | broke into 3 pieces |
| | 13 | 31B | 10 ⁻¹ /sec | 82.1 | 11907.6198 | | 5.7 | 9.519 | 9.513 | 9.489 | 9.507 | 9.489 | 9.519 | 0.030 | break at the bond, seperate bond cookie | broke into 3 pieces |
| | 14 | 18B | 10 ⁻¹ /sec | 84.3 | 12226.7034 | | 5.9 | 9.492 | 9.446 | 9.455 | 9.464 | 9.446 | 9.492 | 0.046 | Bond is intact. Failed at gauge two places | broke into 3 pieces |
| | 15 | 79B | 10 ⁻¹ /sec | 119.1 | 17274.0258 | | 8.3 | 9.54 | 9.537 | 9.551 | 9.543 | 9.537 | 9.551 | 0.014 | break at bond and shattered | broke into 6 pieces |
| | | | ave | 96.48 | 13993.27 | 6.72 | 6.72 | | | | 9.486 | | | | | |
| F | 16 | 115 | 10 ⁻¹ /sec | 94.3 | 13677.0834 | | 6.6 | 9.547 | 9.51 | 9.483 | 9.513 | 9.483 | 9.547 | 0.064 | Broke in gauge both ends | broke into 3 pieces |
| | 17 | 123 | 10 ⁻¹ /sec | 129.3 | 18753.4134 | | 9 | 9.522 | 9.524 | 9.493 | 9.513 | 9.493 | 9.524 | 0.031 | broke at root both ends and shattered | broke into 7 pieces |
| | 18 | 149 | 10 ⁻¹ /sec | 127.4 | 18477.8412 | | 8.9 | 9.546 | 9.514 | 9.525 | 9.528 | 9.514 | 9.546 | 0.032 | broke at root both ends and shattered | broke into 7 pieces |
| | 19 | 150 | 10 ⁻¹ /sec | 87.3 | 12661.8174 | | 6.1 | 9.478 | 9.457 | 9.476 | 9.470 | 9.457 | 9.478 | 0.021 | Broke in gauge one end | broke into 2 pieces |
| | 20 | 163 | 10 ⁻¹ /sec | 131.9 | 19130.5122 | | 9.2 | 9.521 | 9.553 | 9,537 | 9.537 | 9.521 | 9.553 | 0.032 | broke at root both ends and shattered | broke into 5 pieces |

Lofagures 5. Data summary from 10^{s1}/s strain rate Physics



Tests of RPT PMMA

September-07

Comparison between bonded and non-bonded PMMA dumbbells Strain rate of 10-3/sec

30% RH

22 C, 10-3/s

Average Force reg

| Experimental Run | Sample # | Dumbbell # | Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Young's modulus | to break (kN) | Top (mm) | Middle (mm |) Bottom (mm) |) Average (mm) | min(mm) | max(mm) | Delta (mm) | Comments | Comments |
|------------------|----------|------------|-----------------------|------------------------|------------------------|--------------------|------------------|----------|------------|---------------|----------------|---------|---------|------------|--|---|
| А | 1 | 8B | 10 ⁻³ /sec | 66.8 | 9688.5384 | | 4.51 | 9.443 | 9.36 | 9.4 | 9.401 | 9.360 | 9.443 | 0.083 | failed at the bond | Sample loaded w/ bond down, Bond stayed in long end |
| | 2 | 3B | 10 ⁻³ /sec | 69.8 | 10123.6524 | | 4.81 | 9.483 | 9.444 | 9.498 | 9.475 | 9.444 | 9.498 | 0.054 | failed at the bond | Sample loaded w/ bond down, Bond stayed in long end |
| | 3 | 15B | 10 ⁻³ /sec | 70 | 10152.66 | | 4.82 | 9.536 | 9.549 | 9.531 | 9.539 | 9.531 | 9.549 | 0.018 | failed at the bond | Sample loaded w/ bond down, Bond stayed in long end |
| | 4 | 73B | 10 ⁻³ /sec | 71.2 | 10326.7056 | | 4.91 | 9.53 | 9.553 | 9.54 | 9.541 | 9.530 | 9.553 | 0.023 | failed at the bond | Sample loaded w/ bond down, Bond stayed in long end |
| | 5 | 26B | 10 ⁻³ /sec | 64.6 | 9369.4548 | | 4.46 | 9.447 | 9.457 | 9.487 | 9.464 | 9.447 | 9.487 | 0.040 | failed at the bond | Sample loaded w/ bond down, Bond stayed in long end |
| | | | ave | 68.48 | 9932.20 | 3.37 | 4.702 | | | | | | | | | |
| В | 6 | 131 | 10 ⁻³ /sec | 63.5 | 9209.913 | | 4.4 | 9.529 | 9.543 | 9.54 | 9.537 | 9.529 | 9.543 | 0.014 | failed at the tension gauge knife edge | |
| | 7 | 143 | 10 ⁻³ /sec | 73 | 10587.774 | | 5.02 | 9.543 | 9.556 | 9.544 | 9.548 | 9.543 | 9.556 | 0.013 | failed at the center of gauge | |
| | 8 | 120 | 10 ⁻³ /sec | 74.8 | 10848.8424 | | 5.13 | 9.529 | 9.553 | 9.545 | 9.542 | 9.529 | 9.553 | 0.024 | failed at the tension gauge knife edge | |
| | 9 | 108 | 10 ⁻³ /sec | 84.2 | 12212.1996 | | 5.71 | 9.482 | 9.507 | 9.51 | 9.500 | 9.482 | 9.510 | 0.028 | failed at the root of the gauge | |
| | 10 | 130 | 10 ⁻³ /sec | 74.5 | 10805.331 | | 5.11 | 9.526 | 9.556 | 9.543 | 9.542 | 9.526 | 9.556 | 0.030 | failed at the root of the gauge | |
| | | | ave | 74 | 10732.81 | 3.36 | 5.074 | | | | | | | | | |

-40 C, 10-3/sec **Dumbbell Gauge dimensions**

| Experimental Run | Sample # | Dumbbell : | # Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Average Young's modulus | Force req. to break (kN) | Top (mm) | Middle (mm) | Bottom (mm) |) Average (mm) | min(mm) | max(mm) | Delta (mm) | Comments | Comments | |
|------------------|----------|------------|-----------------------|------------------------|------------------------|-------------------------------|--------------------------------|----------|-------------|-------------|----------------|---------|---------|------------|--|---------------------|--|
| A | 1 | 21B | 10 ⁻³ /sec | 92.7 | 13445.0226 | | 6.4 | 9.503 | 9.504 | 9.507 | 9.505 | 9.503 | 9.507 | 0.004 | single break at the bond, bond stayed with the short end | broke into 2 pieces | |
| | 2 | 25B | 10 ⁻³ /sec | 80.8 | 11719.0704 | | 5.6 | 9.52 | 9.506 | 9.528 | 9.518 | 9.506 | 9.528 | 0.022 | single break at the bond, bond stayed with the short end | broke into 2 pieces | |
| | 3 | 76B | 10 ⁻³ /sec | 99.8 | 14474.7924 | | 6.9 | 9.531 | 9.5 | 9.518 | 9.516 | 9.500 | 9.531 | 0.031 | break at the bond, seperate bond cookie | broke into 3 pieces | |
| | 4 | 14B | 10 ⁻³ /sec | 101.6 | 14735.8608 | | 7.1 | 9.502 | 9.528 | 9.517 | 9.516 | 9.502 | 9.528 | 0.026 | single break at the bond, bond stayed with the long end | broke into 2 pieces | |
| | 5 | 46B | 10 ⁻³ /sec | 95.2 | 13807.6176 | | 6.6 | 9.472 | 9.474 | 9.527 | 9.491 | 9.472 | 9.527 | 0.055 | break at the bond, seperate bond cookie | broke into 3 pieces | |
| | | | ave | 94.02 | 13636.47 | 5.42 | 6.52 | | | | 9.509 | | | | | | |
| В | 6 | 139 | 10 ⁻³ /sec | 103.6 | 15025.9368 | | 7.2 | 9.551 | 9.565 | 9.557 | 9.558 | 9.551 | 9.565 | 0.014 | Failed at root of one end | broke into 2 pieces | |
| | 7 | 144 | 10 ⁻³ /sec | 104.1 | 15098.4558 | | 7.2 | 9.533 | 9.529 | 9.543 | 9.535 | 9.529 | 9.543 | 0.014 | Failed at root of one end | broke into 2 pieces | |
| | 8 | 133 | 10 ⁻³ /sec | 106.7 | 15475.5546 | | 7.4 | 9.497 | 9.516 | 9.527 | 9.513 | 9.497 | 9.527 | 0.030 | Failed at root of one end | broke into 2 pieces | |
| | 9 | 126 | 10 ⁻³ /sec | 107.8 | 15635.0964 | | 7.5 | 9.562 | 9.568 | 9.557 | 9.562 | 9.557 | 9.568 | 0.011 | Failed at root of one end | broke into 2 pieces | |
| | 10 | 151 | 10 ⁻³ /sec | 103.6 | 15025.9368 | | 7.2 | 9.535 | 9.543 | 9.546 | 9.541 | 9.535 | 9.546 | 0.011 | Failed at root of one end | broke into 2 pieces | |
| | | | ave | 105.16 | 15252.20 | 5.75 | 7.3 | | | | 9.542 | | | | | | |

Dumbbell Gauge dimensions -90C, 10-3/sec

| | | | | Tensile | Tensile | Average Young's | to break | | | | | | | | | |
|------------------|----------|------------|-----------------------|-------------|-------------|--------------------|----------|----------|------------|--------------|----------------|-------|-------|------------|---|---------------------|
| Experimental Run | Sample # | Dumbbell # | Strain Rate | Yield (Mpa) | Yield (PSI) | modulus | (kN) | Top (mm) | Middle (mm |) Bottom (mm |) Average (mm) | | | Delta (mm) | Comments | Comments |
| С | 11 | 23B | 10 ⁻³ /sec | 110.3 | 15997.6914 | | 7.7 | 9.489 | 9.492 | 9.505 | 9.495 | 9.489 | 9.505 | 0.016 | break at the bond, seperate bond cookie | broke into 3 pieces |
| | 12 | 33B | 10 ⁻³ /sec | 110.5 | 16026.699 | | 7.7 | 9.491 | 9.507 | 9.515 | 9.504 | 9.491 | 9.515 | 0.024 | Bond intact. Failed at two ends | broke into 5 pieces |
| | 13 | 36B | 10 ⁻³ /sec | 111.5 | 16171.737 | | 7.8 | 9.509 | 9.491 | 9.484 | 9.495 | 9.484 | 9.509 | 0.025 | break at the bond, seperate bond cookie | broke into 3 pieces |
| | 14 | 6B | 10 ⁻³ /sec | 97.2 | 14097.6936 | | 6.8 | 9.454 | 9.499 | 9.418 | 9.457 | 9.418 | 9.499 | 0.081 | single break at the bond, bond stayed with the long end | broke into 2 pieces |
| | 15 | 4B | 10 ⁻³ /sec | 116 | 16824.408 | | 8.1 | 9.54 | 9.566 | 9.549 | 9.552 | 9.540 | 9.566 | 0.026 | Bond intact. Failed at root one end | broke into 2 pieces |
| | | | ave | 109.1 | 15823.65 | 6.53 | 7.62 | | | | 9.501 | | | | | |
| | | | | | | | | | | | | | | | | |
| D | 16 | 129 | 10 ⁻³ /sec | 107.8 | 15635.0964 | | 7.5 | 9.469 | 9.557 | 9.547 | 9.524 | 9.469 | 9.557 | 0.088 | Broke at root and in gauge | broke into 4 pieces |
| | 17 | 114 | 10 ⁻³ /sec | 115.4 | 16737.3852 | | 8.2 | 9.528 | 9.557 | 9.544 | 9.543 | 9.528 | 9.557 | 0.029 | Broke at root both ends | broke into 3 pieces |
| | 18 | 136 | 10 ⁻³ /sec | 116.3 | 16867.9194 | | 8.1 | 9.533 | 9.536 | 9.529 | 9.533 | 9.529 | 9.536 | 0.007 | Broke at root both ends | broke into 3 pieces |
| | 19 | 116 | 10 ⁻³ /sec | 115 | 16679.37 | | 8 | 9.557 | 9.568 | 9.556 | 9.560 | 9.556 | 9.568 | 0.012 | Failed at root of one end | broke into 2 pieces |
| | 20 | 146 | 10 ⁻³ /sec | 119.3 | 17303.0334 | | 8.3 | 9.536 | 9.541 | 9.532 | 9.536 | 9.532 | 9.541 | 0.009 | Broke at root both ends | broke into 5 pieces |
| | | | 21/0 | 114 76 | 16644 E6 | 6 E0 | 0.02 | | | | 0.520 | | | | | |

Dumbbell Gauge dimensions -130C, 10-3/sec

| Experimental Run | Sample # | Dumbbell # | Strain Rate | Tensile Yield (Mpa) | Tensile Yield (PSI) | Young's modulus | to break (kN) | Top (mm) | Middle (mm |) Bottom (mn | ı) Average (mm) | min (mm) | max(mm) | Delta (mm) | Comments | Comments |
|------------------|----------|------------|-----------------------|------------------------|------------------------|--------------------|------------------|----------|------------|--------------|-----------------|----------|---------|------------|--|---------------------|
| G | 11 | 27B | 10 ⁻³ /sec | 96.4 | 13981.6632 | · | 6.7 | 9.522 | 9.499 | 9.468 | 9.496 | 9.468 | 9.522 | 0.054 | break at bond and bond stayed with the long end | broke into 2 pieces |
| | 12 | 20B | 10 ⁻³ /sec | 96.2 | 13952.6556 | | 6.7 | 9.518 | 9.547 | 9.491 | 9.519 | 9.491 | 9.547 | 0.056 | Bond is intact. Failed at gauge in one place | broke into 2 pieces |
| | 13 | 40B | 10 ⁻³ /sec | 70 | 10152.66 | | 4.9 | 9.528 | 9.54 | 9.502 | 9.523 | 9.502 | 9.540 | 0.038 | Bond is intact. Failed at gauge in one place | broke into 2 pieces |
| | 14 | 41B | 10 ⁻³ /sec | 113.21 | 16419.752 | | 7.9 | 9.485 | 9.452 | 9.508 | 9.482 | 9.452 | 9.508 | 0.056 | Bond is intact. Failed at gauge in one place | broke into 2 pieces |
| | 15 | 78B | 10 ⁻³ /sec | 70.7 | 10254.1866 | | 5 | 9.534 | 9.534 | 9.544 | 9.537 | 9.534 | 9.544 | 0.010 | break at bond and bond stayed with the short end | broke into 2 pieces |
| | | | ave | 89.302 | 12952.18 | 6.73 | 6.24 | | | | 9.511 | | | | | |
| Н | 16 | 157 | 10 ⁻³ /sec | 80.5 | 11675.559 | | 5.6 | 9.555 | 9.557 | 9.542 | 9.551 | 9.542 | 9.557 | 0.015 | Broke in gauge one end | broke into 2 pieces |
| | 17 | 118 | 10 ⁻³ /sec | 84.9 | 12313.7262 | | 5.9 | 9.52 | 9.518 | 9.536 | 9.525 | 9.518 | 9.536 | 0.018 | broke at root and gauge and shattered | broke into 5 pieces |
| | 18 | 161 | 10 ⁻³ /sec | 106.1 | 15388.5318 | | 7.4 | 9.5 | 9.536 | 9.505 | 9.514 | 9.500 | 9.536 | 0.036 | broke in gauge two places | broke into 3 pieces |
| | 19 | 141 | 10 ⁻³ /sec | 110.5 | 16026.699 | | 7.7 | 9.54 | 9.566 | 9.511 | 9.539 | 9.511 | 9.566 | 0.055 | broke at root and gauge two places | broke into 3 pieces |
| | 20 | 103 | 10 ⁻³ /sec | 74.7 | 10834.3386 | | 5.2 | 9.506 | 9,505 | 9,503 | 9.505 | 9,503 | 9.506 | 0.003 | Broke in gauge one end | broke into 2 pieces |

Lofagures Data summary from 10⁵³/s strain rate Physics



A quicktime movie of a breaking sample.

